Photoacoustic imaging through a cortical bone replica with anisotropic elasticity

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Photoacoustic (PA) imaging is an emerging modality which combines the high optical absorption contrast of biological chromophores with centimeter imaging depths and sub-millimeter resolution of ultrasonic (US) waves. However, PA imaging through cortical bone remains an unmet challenge. Cortical bone is an anisotropic medium which is not accurately modeled with existing PA image reconstruction methods. In this Letter, we address the PA source localization problem for imaging through a cortical bone-mimicking layer. Our approach accounts for both refraction and elastic anisotropy to accurately reconstruct an US and PA image in the presence of a cortical bone replica. We demonstrate our technique with a PA and US experiment, where we image a 700 µm diameter target beneath a cortical bone-mimicking plate. Pulse-echo US is used to estimate the wavespeed in each layer and create an anatomical image of the bone replica, and the PA source is reconstructed in reception-only using the wavespeed model defined with US. We compute the thickness of the plate with less than 1% error, whereas isotropic assumptions overestimate the thickness by 20% or more. Incorporating both refraction and anisotropy accurately localizes the target with PA and US at the true depth, whereas isotropic assumptions blur the lateral dimension and mislocate the target depth by 1.5-4 mm.

Photoacoustic (PA) imaging is capable of generating high-contrast images of blood vessels non-invasively using the endogenous contrast of hemoglobin in the blood stream1,2. In reflection/epi-mode, a nanosecond pulse of diffuse light is absorbed by hemoglobin, creating a transient pressure rise which propagates as an ultrasonic “PA” wave to the tissue surface where it recorded by ultrasonic (US) detectors. Reconstructing the origin of the PA source creates images of optical absorption contrast with US resolution at multiple centimeter imaging depths.

However, mainstream PA reconstruction methods3–5 approximate all tissues as an isotropic, homogeneous fluid and cannot image beyond the first interface of bone (periostium). The PA rays are assumed to travel in straight lines from the source (optical absorber) to receiver (US probe). This assumption is reasonable for soft-tissues, but breaks down in the presence of bone, which is an anisotropic material6–8 with a higher wavespeed than soft-tissues. In reality, PA rays refract upon crossing into and out of cortical bone, and experience an anisotropic wavespeed within cortical bone, as shown in Fig. 1.

Non-invasive detection of PA signals in the human brain has been shown9, demonstrating that sufficient light penetrates through a bone layer to generate measurable PA signals. However, PA imaging through a bone layer has not yet been shown. Recent work has successfully removed aberrations in numerical and experimental phantom data due to PA wave propagation through an isotropic skull model toward the goal of transcranial PA imaging10,11. However, a known, isotropic wavespeed model is assumed and must be found with X-ray computed tomography (CT)12. Isotropic assumptions based on CT scans are also used for transcranial US therapy12,13. While these examples focus on measurement, therapy, and imaging through the skull (cancellous bone), the challenges for imaging through cortical bone are related. In cortical bone, the preferential orientation of pores and mineralized fibrils result in an anisotropic wavespeed distribution in the longitudinal plane, where the wavespeed is more than 20% higher along the bone diaphysis (axial direction) than in the radial direction perpendicular to the diaphysis8. Therefore, isotropic wavespeed assumptions are insufficient for accurate imaging in the presence of cortical bone14.

In this Letter, we present a methodology which accounts for both refraction and elastic anisotropy to address the acoustic source localization problem for PA imaging beneath a cortical bone-mimicking layer with anisotropic elasticity. US data are acquired along with the PA data to measure the wavespeed model and create anatomical US images of the bone layer without the aid of an external modality, such as CT. US and PA data are routinely acquired concurrently with dual-modality systems15,16, and in human US imaging of the bone cortex has recently been demonstrated14,17.

The experimental setup is shown in Fig. 1. An 8 mm cortical bone-mimicking plate is suspended in a water bath above an optically absorbing target (700 µm diameter graphite rod). The bottom of the rod is located at a depth of 23 mm. The plate thickness is on the order of the thickness of the posterior cortex of a human femur18, where the effects of anisotropy and refraction would be especially pronounced. The bone plate (Sawbones, Pacific Research Laboratory Inc, Vashon WA) has been studied previously, and found to have similar elastic properties to human cortical bone19. In particular, both Sawbones and cortical bone are transverse-isotropic2. The

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wavespeed is isotropic in the transverse plane perpendicular to the material fibril orientation, and anisotropic in the longitudinal plane parallel to the fibers (Fig. 2).

Water is used to approximate the cutaneous tissue and bone marrow layers. Soft-tissue (acoustic) approximations are good approximations for these tissues\(20\), though the magnitude of the wavespeed in the cutaneous tissues and bone marrow will differ \textit{in vivo}\(21\). The plate is optically opaque, therefore we illuminate the PA target below the plate with a nanosecond pulsed laser coupled to an optical fiber bundle (OPOTEK Radiant 532 LD). The laser wavelength is 680 nm with a pulse width of 5 ns, 20 Hz repetition rate, and energy density \(\sim 10 \text{ mJ/cm}^2\). Optical illumination considerations for non-invasive \textit{in vivo} PA imaging in bone are detailed at the end of the Letter.

Both US and PA data were acquired using a programmable US probe (L11-5v, 7.6 MHz center frequency) and an ultrafast US system (Varian, Vantage 128). In a preliminary experiment, we acquired data in both the longitudinal (anisotropic) and transverse (isotropic) plane to compute the wavespeed model in the bone plate. Each element was independently fired, and the resulting wavefield was recorded on all elements simultaneously to create an inter-element matrix. The axial wavespeed \(V_a\), radial wavespeed \(V_r\), and anisotropic form parameter \(\beta\) of the bone plate are computed using the procedure detailed in Ref. 14, with one variation. To compute the headwave speed along the axial direction, we apply a linear-moveout correction\(^{22,23}\) in the time-domain rather than the frequency domain approach described in Ref. 14. All elastic properties are computed automatically given wavespeed bounds and depth parameters as inputs, and listed in Table I. For imaging, we acquired PA data as well as a complete inter-element US matrix in the longitudinal plane. Mode-converted shear waves and surface-related multiple reflections are muted in the raw US data.

Delay-and-sum (DAS) beamforming for US imaging computes travel times between two points in a 2D medium with coordinates \((x_1, z_1)\) and \((x_2, z_2)\) with the distance equation:

\[
t = \frac{\sqrt{(x_1 - x_2)^2 + (z_1 - z_2)^2}}{V},
\]

assuming a constant wavespeed \(V\). In soft-tissues, \((x_1, z_1)\) is normally fixed as the coordinates of an array element and \((x_2, z_2)\) is the coordinates of an image pixel \(p\).

The US image \((I_{US})\) is then computed

\[
I_{US}(p) = \sum_{i=1}^{M} \sum_{j=1}^{N} W(p, i, j) \times D_{US}[t = t_R(i, p) + t_R(j, p), i, j],
\]

where the image at each pixel \(p\) is the summation of wavefield data \(D_{US}\) recorded at time \(t\) for a single emitter \(i\) and receiver \(j\). The total travel time is the summation of transmit times \(t_T\) for a ray travelling from \(i\) to \(p\), and receive times \(t_R\) for a ray travel from \(p\) to \(j\) (Fig. 1). The one-way propagation time for a PA wave generated by a source at \(p\) which propagates to \(j\) is equivalent to \(t_R\) computed in the US reconstruction. Therefore, a PA image is computed:

\[
I_{PA}(p) = \sum_{j=1}^{N} W(p, j) \times D_{PA}[t = t_R(j, p)],
\]

Each data point in \(D_{US}\) and \(D_{PA}\) is multiplied by a weighting factor \(W\) to reduce side lobe artifacts. Data outside of a predefined acceptance angle are multiplied by zero, and within the acceptance angle are multiplied by 1.

\begin{table}[h]
\centering
\begin{tabular}{|c|c|c|c|c|}
\hline
& \(V_{lens}\) & \(V_{water}\) & \(V_a\) & \(V_r\) & \(\beta\) \\
\hline
\text{US} & 1003 m/s & 1486 m/s & 3843 m/s & 3032 m/s & 1.95 \\
\hline
\end{tabular}
\caption{Elastic properties used for the image reconstruction.}
\end{table}
For bone, the travel-times must be adjusted for the true propagation times through the higher-wavespeed, anisotropic cortical bone. To achieve this, we implement a modified DAS approach based on Kirchhoff migration\textsuperscript{24} which incorporates both refraction and elastic anisotropy.

First, we reconstruct an US image layer-by-layer\textsuperscript{14,17}. For each layer, we compute both $t_r$ and $t_k$ using identical methods, therefore we discuss $t_r$ exclusively in the following.

An US image in the cutaneous tissue (water) layer is computed to a predefined depth. The travel times in the water layer are computed assuming both the silicone lens and water are isotropic, homogeneous fluids with wavespeeds listed in Table I. At the (known) lens-water interface, we apply Snell’s law which refracts the ray according to the acoustic impedance and emerging angle $\phi_r$. With these travel times, the US image of the water layer is reconstructed using Eq. 2.

The brightest reflector in this water layer is the first bone interface, which is segmented with the Dijkstra algorithm\textsuperscript{25,26} and fit to a parabola.

Within the cortical bone layer, refraction and anisotropy must be taken into account. Each ray begins at an emitter $i$, and Eq. 1 is first applied through the lens and tissue layer. When a ray reaches a pixel on the parabola corresponding to the water-bone interface, refraction is enforced according to the acoustic impedance between the water layer and bone, and the ray changes direction according to Snell’s law from $\phi_r$ to $\theta$ as in Fig. 1. Within the bone layer, Eq. 1 is applied, but now $(x_1, z_1)$ corresponds to the point on the interface. Further, the anisotropic (angle-dependent) group wavespeed $V_B(\theta)$ replaces $V$. To compute $V_B(\theta)$, we use Thomsen’s equation for weak anisotropy\textsuperscript{27}:

\begin{equation}
V_B(\theta) = V_a - (V_a - V_r) \times \left[ \beta \sin^2 \theta \cos^2 \theta + \cos^4 \theta \right], \tag{4}
\end{equation}

as shown in Fig. 3 using the properties listed in Table I. A range of $\phi_r$ are tested, until the minimum travel time from $i$ to $p$ within the bone layer is found. With these travel times incorporating refraction and anisotropy, Eq. 2 is used to compute the bone layer as in standard DAS.

Next, we segment and fit a parabola to the bone-water interface, the brightest reflector in the bone layer. For the marrow (water) layer, we follow an identical procedure to the bone layer, but this time following a ray from $i$, through the first interface and bone layer, and enforce refraction a second time at the bone-water interface. Within the marrow layer, an isotropic wavespeed $V_{\text{water}}$ is used. Finally, after computation of $t_r$ and $t_k$ in the US reconstruction, we reconstruct the PA image with Eq. 3.

PA and US imaging results using conventional DAS and our bone imaging approach assuming both an isotropic and anisotropic wavespeed in bone are shown in Fig. 4. The US image is Hilbert transformed and log compressed for display. All non-positive values in the PA image are thresholded to zero\textsuperscript{28}, and the PA image is normalized and overlaid onto the US image in red.

The lateral and depth dimension across the peak corresponding to the top of the target measured with PA and US, as well as the thickness of the bone layer computed with US are reported in Table II. Generated PA and scattered US signals are observed from both the top and bottom of the target, along with reverberations. Therefore the dimensions are measured for the signal from the top of the target only. The dimensions are measured by normalizing the marrow image (without log compression) and extracting perpendicular cross sections across the peak corresponding to the top of the target in the image. Cross-sections are upsampled by a factor of 10, and the width of the peak at $-10$ dB is measured.

In Fig. 4(a), a DAS algorithm assuming a homogeneous, isotropic medium ($V = V_{\text{water}}$) is used. The target is unfocused and the depth is largely underestimated with both PA and US. The interfaces of the bone plate are also improperly mapped, and the thickness is underestimated by $\sim 29\%$. In Fig. 4(b), we utilise our refraction-based approach with an isotropic wavespeed model for the bone plate, where the optimum wavespeed ($3677 \text{ m s}^{-1}$) in bone is chosen by optimising the image quality\textsuperscript{29}. The thickness of the plate is overestimated by $\sim 20\%$. While the target is better focused in Fig. 4(b) than Fig. 4(a), it is located at the wrong depth and the lateral diameter is blurred in both PA and US images. In Fig 4(c), the true thickness of the plate is found to be $7.96 \pm 0.02 \text{ mm}$. The lateral dimension at $-10$ dB is smallest when utilising the anisotropic model for both PA and US and the target is located within $100 \mu\text{m}$ of the true depth.

In our phantom experiment, the angle of optical illumination is such that the light avoids propagation through the opaque bone-mimicking replica. For \textit{in vivo} PA imaging, optical transmission through soft-tissue and bone will be hampered by intrinsic losses, but recording PA signals through a bone layer has already proven feasible \textit{in vivo}\textsuperscript{9}. Consider a model with 5 mm of cutaneous soft-tissue and a cortical bone thickness ranging from $4 \text{ mm}$ typical of a human radius, to the thicker cortex of the human femur ($\sim 8 \text{ mm}$). The effective optical attenuation coefficient $\mu_{\text{eff}}$ in soft-tissue within the optical window is\textsuperscript{1} $\sim 0.13 \text{ mm}^{-1}$, therefore, the initial fluence will reduce by $\sim 50\%$ through the soft-tissue layer. In bone, we approximate\textsuperscript{30} $\mu_{\text{eff}} \sim 0.17 \text{ mm}^{-1}$, reducing the fluence by another $50\%$ through a $4 \text{ mm}$ bone layer and $75\%$ through an $8 \text{ mm}$ layer. For an initial fluence of $20 \text{ mJ cm}^2$, the fluence remaining in the bone marrow of the radius will be $\sim 5 \text{ mJ cm}^2$ and in the femur $\sim 2.5 \text{ mJ cm}^2$, sufficient for measurable PA generation. Accounting for loss-of-energy due to reflection of the US and PA waves, optical and acoustic attenuation, we estimate that PA imaging beneath $5 \text{ mm}$ of soft-
FIG. 4. US (grayscale) and PA (red overlay) images reconstructed using (a) DAS assuming a constant wavespeed of $V_{\text{water}} = 1486 \text{ m/s}$ and refraction-corrected imaging with a (b) layered medium including a bone layer with isotropic elasticity and (c) layered medium including a bone layer with anisotropic elasticity. The interfaces segmented in the US image using the method in (c) are shown with a dotted green line on all three panels. The true location of the top of the target is marked ‘X’. Cross-sections along the lateral and depth direction are extracted at the point in the PA (dotted red lines) and US (white lines) images corresponding to the top of the target. The PA and US cross sections are shown in red and black, respectively. The width at $-10 \text{ dB}$ of each cross section is denoted with arrows.

<table>
<thead>
<tr>
<th>wavespeed model</th>
<th>uniform medium:</th>
<th>layered medium:</th>
<th>layered medium:</th>
<th>ground truth</th>
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<tr>
<td>thickness cortical bone replica</td>
<td>“soft-tissue”</td>
<td>bone layer, isotropic elasticity</td>
<td>bone layer, anisotropic elasticity</td>
<td>ground truth</td>
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<tr>
<td>PA target depth (top)</td>
<td>5.67 mm</td>
<td>9.62 mm</td>
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<td>7.97 mm</td>
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<td>US target depth (top)</td>
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<td>22.3 mm</td>
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<td>PA dimensions (lateral, depth)</td>
<td>3383 µm, 156 µm</td>
<td>1354 µm, 176 µm</td>
<td>924 µm, 161 µm</td>
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<tr>
<td>US dimensions (lateral, depth)</td>
<td>4331 µm, 386 µm</td>
<td>1589 µm, 396 µm</td>
<td>797 µm, 416 µm</td>
<td>–</td>
</tr>
</tbody>
</table>

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REFERENCES


